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Since $E_1 = 3.06$ m, the above relation gives

$$3.06 = \frac{3}{2} \left[\frac{(20/b)^2}{9.81} \right]^{1/3}$$

which yields b = 2.19 m. Therefore, the minimum allowable width of the constriction to prevent choking in 2.19 m.

3.36. From the given data: $Q = 36 \text{ m}^3/\text{s}$, b = 10 m, n = 0.030, $S_o = 0.001$, and y = 3 m. Determine the normal depth, using the Manning equation

$$Q = \frac{1}{n} \frac{A^{5/3}}{P^{2/3}} \sqrt{S_o}$$

36 = $\frac{1}{0.030} \frac{(10y_n)^{5/3}}{(10+2y_n)^{2/3}} \sqrt{0.001}$

which gives

$$y_n = 2.45 \text{ m}$$

Determine the critical depth,

$$y_c = \left(\frac{q^2}{g}\right)^{1/3} = \left(\frac{3.6^2}{9.81}\right)^{1/3} = 1.09 \text{ m}$$

Since $y > y_n > y_c$, the water surface follows a M1 profile. Determine S_f using the Manning equation,

$$S_f = \left[\frac{nQ}{AR^{2/3}}\right]^2 = \left[\frac{nQP^{2/3}}{A^{5/3}}\right]^2 = \left[\frac{nQ(10+2y)^{2/3}}{(10y)^{5/3}}\right]^2 = \left[\frac{(0.030)(36)(10+2\times3)^{2/3}}{(10\times3)^{5/3}}\right]^2 = 0.00056$$

The slope of the water surface is given by

$$\frac{dy}{dx} = \frac{S_o - S_f}{1 - Fr^2} = \frac{0.001 - 0.00056}{1 - \left(\frac{1.2}{9.81(3)}\right)^2} = \boxed{0.00046}$$

where the velocity is taken as $V = Q/A = 36/(10 \times 3) = 1.2$ m/s.

If y = 2 m, then $y_n > y > y_c$ and the water surface follows a M2 profile. Therefore the shape of the water surface would be different than when y = 3 m.

3.37. From the given data: $Q = 30 \text{ m}^3/\text{s}$, b = 8 m, and n = 0.035.

$$y_c = \left[\frac{q^2}{g}\right]^{1/3} = \left[\frac{(30/8)^2}{9.81}\right]^{1/3} = 1.13 \text{ m}$$

$$S_c = \left[\frac{nQP^{2/3}}{A^{5/3}}\right]^2 = \left[\frac{nQ(8+2y_c)^{2/3}}{(8y_c)^{5/3}}\right]^2 = \left[\frac{(0.035)(30)(8+2\times1.13)^{2/3}}{(8\times1.13)^{5/3}}\right]^2 = 0.016$$

Hence for Mild Slope: $0 < S_o < 0.016$ and for Steep Slope: $S_o > 0.016$.

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3.38. From given data: b = 6 m, m = 2, n = 0.045, $S_o = 0.015$, Q = 80 m³/s, and y = 5 m. Calculate normal depth using Manning equation,

$$Q = \frac{1}{n} \frac{A^{5/3}}{P^{2/3}} \sqrt{S_o}$$

80 = $\frac{1}{0.045} \frac{(by_n + 2y_n^2)^{5/3}}{(b + 2\sqrt{5}y_n)^{2/3}} \sqrt{S_o} = \frac{1}{0.045} \frac{(6y_n + 2y_n^2)^{5/3}}{(6 + 2\sqrt{5}y_n)^{2/3}} \sqrt{0.015}$

which gives

$$y_n = 2.21 \text{ m}$$

Calculate the critical depth,

$$\frac{Q^2}{g} = \frac{A_c^3}{T_c}$$
$$\frac{80^2}{9.81} = \frac{(by_c + 2y_c^2)^3}{(b+4y_c)}$$
$$652.4 = \frac{(6y_c + 2y_c^2)^3}{(6+4y_c)}$$

which gives

$$y_c = 2.07 \text{ m}$$

Since $y > y_n > y_c$, the water surface has a M1 profile and the depth increases in the downstream direction.

The slope, S_f , of the energy grade line is given by the Manning equation as

$$S_f = \left[\frac{nQP^{2/3}}{A^{5/3}}\right]^2 = \left[\frac{nQ(b+2\sqrt{5}y)^{2/3}}{(by+2y^2)^{5/3}}\right]^2 = \left[\frac{(0.045)(80)(6+2\sqrt{5}\times5)^{2/3}}{(6\times5+2\times5^2)^{5/3}}\right]^2 = 0.000508$$

Other hydraulic parameters are

$$A = by + 2y^{2} = (6)(5) + 2(5)^{2} = 80 \text{ m}^{2}$$

$$V = \frac{Q}{A} = \frac{80}{80} = 1 \text{ m/s}$$

$$T = b + 2my = (6) + 2(2)(5) = 26 \text{ m}$$

$$D = \frac{A}{T} = \frac{80}{26} = 3.08 \text{ m}$$

$$Fr^{2} = \frac{V^{2}}{gD} = \frac{1^{2}}{9.81(3.08)} = 0.0331$$

The slope of the water surface is therefore given by

$$\frac{dy}{dx} = \frac{S_o - S_f}{1 - Fr^2} = \frac{0.015 - 0.000508}{1 - 0.0331} = \boxed{0.0150}$$

The depth, y_u , 100 m upstream is given by

$$y_u = 5 - 100(0.0150) = |3.50 \text{ m}|$$

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and the depth, y_d , 100 m downstream is given by

$$y_u = 5 + 100(0.0150) = 6.50 \text{ m}$$

3.39. According to the momentum equation

$$\sum F_x = \rho Q(V_2 - V_1)$$

In this case,

$$\gamma A_1 \bar{y}_1 - \gamma A_2 \bar{y}_2 + \gamma \mathcal{V} \sin \theta = \rho Q \left(\frac{Q}{A_2} - \frac{Q}{A_1} \right)$$
$$A_1 \bar{y}_1 - A_2 \bar{y}_2 + \mathcal{V} \sin \theta = Q \left(\frac{Q}{gA_2} - \frac{Q}{gA_1} \right)$$

For a rectangular channel of width b,

$$A_1 = by_1$$

$$A_2 = by_2$$

$$\bar{y}_1 = \frac{y_1}{2}$$

$$\bar{y}_2 = \frac{y_2}{2}$$

$$\mathcal{V} = \frac{y_1 + y_2}{2} 5y_2 b$$

$$\sin \theta = S_o$$

$$Q = qb$$

and substituting into the momentum equation gives

$$b\frac{y_1^2}{2} - b\frac{y_2^2}{2} + \frac{y_1 + y_2}{2}5y_2bS_o = \frac{q^2b^2}{gby_2} - \frac{q^2b^2}{gby_1}$$
$$\frac{y_1^2}{2} - \frac{y_2^2}{2} + \frac{y_1 + y_2}{2}5y_2S_o = \frac{q^2}{gy_2} - \frac{q^2}{gy_1}$$

or

$$\frac{y_1^2}{2} + \frac{q^2}{gy_1} = \frac{y_2^2}{2} + \frac{q^2}{gy_2} - \frac{y_1 + y_2}{2} 5y_2 S_o$$

3.40. From given data: $Q = 100 \text{ m}^3/\text{s}, b = 8 \text{ m}, y_1 = 0.9 \text{ m}, \text{ and}$

$$q = \frac{Q}{b} = \frac{100}{8} = 12.5 \text{ m}^2/\text{s}$$

and

$$y_2 = \frac{y_1}{2} \left(-1 + \sqrt{1 + 8 \text{Fr}_1^2} \right)$$
$$= \frac{y_1}{2} \left(-1 + \sqrt{1 + 8 \frac{q^2}{gy_1^3}} \right) = \frac{0.9}{2} \left(-1 + \sqrt{1 + 8 \frac{12.5^2}{(9.81)(0.9)^3}} \right) = \boxed{5.52 \text{ m}}$$