$$
\begin{aligned}
\frac{1}{n_{e}} \frac{A^{5 / 3}}{P^{2 / 3}} & =\sum_{i=1}^{N} \frac{1}{n_{i}} \frac{A_{i}^{5 / 3}}{P_{i}^{2 / 3}} \\
\frac{1}{n_{e}} P R^{5 / 3} & =\sum_{i=1}^{N} \frac{1}{n_{i}} P_{i} R_{i}^{5 / 3}
\end{aligned}
$$

which simplifies to

$$
n_{e}=\frac{P R^{5 / 3}}{\sum_{i=1}^{N} \frac{P_{i} R_{i}^{5 / 3}}{n_{i}}}
$$

3.19. From the given shape of the floodplain (Figure 3.5), the following geometric characteristics are derived:

| Section, $i$ | $\|c\| c$ <br> $P_{i}$ <br> $(\mathrm{~m})$ | $A_{i}$ <br> $\left(\mathrm{~m}^{2}\right)$ | $R_{i}$ <br> $(\mathrm{~m})$ | $n_{i}$ | $y_{i}$ <br> $(\mathrm{~m})$ |
| :---: | ---: | ---: | :---: | :---: | :---: |
| 1 | 20.6 | 50 | 2.42 | 0.040 | 2.50 |
| 2 | 100.0 | 500 | 5.00 | 0.030 | 5.00 |
| 3 | 6.7 | 39 | 5.81 | 0.015 | 6.50 |
| 4 | 15.0 | 120 | 8.00 | 0.013 | 8.00 |
| 5 | 6.7 | 39 | 5.81 | 0.017 | 6.50 |
| 6 | 150.0 | 750 | 5.00 | 0.035 | 5.00 |
| 7 | 20.6 | 50 | 2.42 | 0.060 | 2.50 |
| 7 | 319.6 | 1548 |  |  |  |

The total perimeter, $P$, of the (compound) channel is 319.6 m , the total area, $A$, is $1548 \mathrm{~m}^{2}$, and hence the hydraulic radius, $R$, of the compound section is given by

$$
R=\frac{A}{P}=\frac{1548}{319.6}=4.84 \mathrm{~m}
$$

Substituting these data into the formulae listed in Table 3.2 yields the following results:

| Formula | $n_{e}$ |
| :--- | :---: |
| Horton/Einstein | 0.034 |
| Muhlhofer/Einstein and Banks | 0.035 |
| Lotter | 0.026 |
| Krishnamurthy and Christensen | 0.029 |
| Average | 0.031 |

A conservative (high) estimate of the composite roughness is 0.035 , and the average composite roughness predicted by the models is 0.031 .
3.20. In the main channel: $n=0.016$ and $S_{o}=0.005$. When the main channel flows full:

$$
\begin{aligned}
A & =\frac{1}{2}[30+30+3(2)+3(3)](3)=112.5 \mathrm{~m}^{2} \\
P & =30+3\left(\sqrt{3^{2}+1^{2}}+\sqrt{2^{2}+1^{2}}\right)=46.2 \mathrm{~m} \\
R & =\frac{A}{P}=\frac{112.5}{46.2}=2.44 \mathrm{~m}
\end{aligned}
$$

